

**SHRINKAGE DEFORMATIONS BETONA IN A DRY HOT CLIMATE**

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Abstract

The article provides an analysis of the deformation of concrete in dry and hot climates. Concrete shrinkage deformations under conditions of dry hot climate have pronounced periodic character depending on seasonal variation of air temperature and humidity.

Keywords: shrinkage, stresses, deformation, humidity, temperature, temperature expansion, wet storage, solar radiation, moisture release of concrete, seasonal change, normal condition.

The climatic conditions of the Republic of Uzbekistan are sharply continental. In summer, the air temperature can exceed + 40°C, while the relative humidity drops to 10-15% and below. In such klimaticheskikh conditions, from direct exposure to solar radiation, the surface of reinforced concrete and concrete structures is heated to 70-80°C. At the same time, significant deformations of concrete shrinkage appear, leading to the formation and opening of cracks on the surface of reinforced concrete and betonnykh structures.

One of the most important factors in improving the reliability and durability of structures of buildings and structures, especially for the Republic of Uzbekistan, is the further improvement of methods for their rascheta taking into account real operating conditions. When concrete hardens in a dry hot climate, the two opposite structural and destructive processes take place. The more structural processes prevail, the deeper and denser the hydration of cement will be, the physical and chemical hardening processes are more intensive, the strength of concrete is gained faster, and concrete is more resistant in hot climates. In the absence of proper care for concrete, dehydration of fresh concrete occurs. Concrete in dry weather during the first day loses 50... 70% of the water of consolidation.

Intensive evaporation of moisture from the surface of freshly laid concrete causes plastic and moisture shrinkage of concrete. Plastic shrinkage of concrete occurs immediately after the formation of the concrete mixture, when it has not yet fully hardened. Plastic shrinkage of concrete causes the formation of surface cracks. Therefore, in order to prevent the evaporation of water from concrete, immediately after molding, moisture care of the concrete should be carried out. Any delay from the beginning of concrete care over 20 ... 30 minutes already contributes to the development of plastic shrinkage of concrete. Humid care of concrete immediately after the completion of the molding of a product or structure reduces the possibility of plastic shrinkage and cracking of exposed surfaces of concrete. The minimum



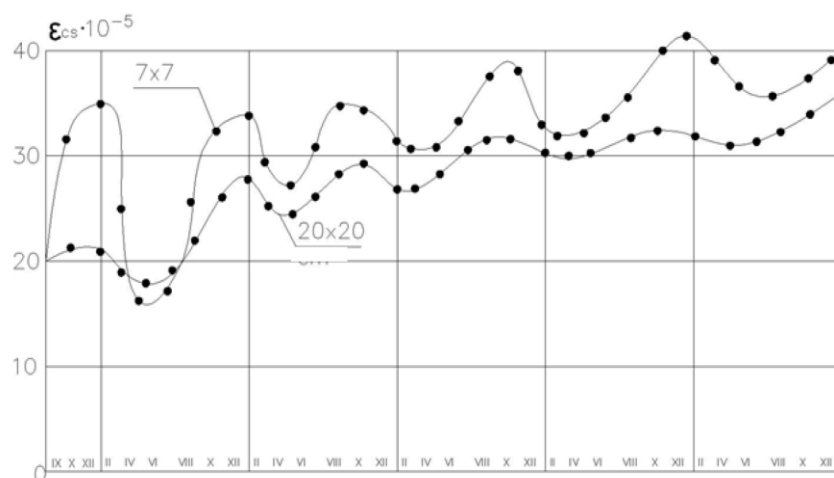
duration of the initial care of freshly laid concrete in order to obtain the least plastic shrinkage in hot dry weather is 6 ... 7 hours.

Further care of concrete does not significantly affect the subsequent development of concrete plastic shrinkage deformation, but it is necessary for the formation of a dense concrete structure and a set of 50 ... 70% compressive strength. Concrete is carefully covered with moisture-proof or damp materials for 8 ... 10 days, the concrete is constantly kept in wet conditions, preventing it from drying out. Under natural conditions of a dry hot climate, humidity deformations of concrete shrinkage develop along a certain cyclic curve damped from seasonal changes in the humidity of the outside air.

In the warm dry season, the greatest development of shrinkage deformations is observed in concrete, which gradually stops its development in the cold wet season and turns into swelling deformations of concrete. However, the swelling deformation is less than the shrinkage deformation of concrete. The amplitude of the cycle of moisture shrinkage and swelling deformations decreases with time, but eventually moisture shrinkage deformations remain in the concrete. The deformations of moisture shrinkage of concrete are the greater, the smaller the section of the element and the lower the relative humidity of the air. The influence of the dimensions of the section of elements on the deformation of concrete shrinkage is most pronounced in the initial periods of operation of the structure. The maximum values of deformation of moisture shrinkage of concrete are observed during the manufacture of the element in the warm dry season. The calculated values of the concrete shrinkage deformation for a given operating time are calculated using a hyperbolic dependence.

$$\varepsilon_{cs} = \varepsilon_{cs1} \frac{\Delta\tau}{\alpha_{cs} + \Delta\tau} \quad (1.1)$$

Where $\Delta\tau$ - time per day. from the end of the wet storage of concrete to the specified service life. Parameter α_{cs} - growth rate of concrete shrinkage strains, the value of which is taken from Table. 1.4 /2.3/ depending on the season of manufacture and the reduced section height.



Rice. 1.1.1. Time development of concrete shrinkage deformations in prisms of cross section 7x7 and 20x20 sm in a dry hot climate.



Table 1.4

Time of year of construction Parameter values for element α_{csc} with reduced section height

Time of year of construction	Parameter values for element α_{csc} with reduced section height h_{red} , (sm) (
	3,5	5,0	10,0	20,0	30,0	40	50
Warm /summer /	15	20	40	80	120	160	200
Cold /winter/	40	60	120	240	360	480	600

Note. In the manufacture of structures other than those indicated in Table. 1.4, the values of the parameter α_{cs} are taken by linear interpolation.

The calculated limit values of concrete shrinkage deformations are calculated based on the relative seasonal (average monthly) air humidity during the construction period. The limiting design values of concrete shrinkage deformations, corresponding to the water consumption of mixing the concrete mixture and the actual operating conditions of the structures, are calculated by the formula.

$$\varepsilon_{cs_1} = \varepsilon_{cs} \cdot \varphi_n \cdot \varphi_w \quad (1.2)$$

The value of the coefficient φ_n is found in Table. 1.3 depending on the season of manufacture of the structure and the reduced sectional height. The value of the calculated concrete shrinkage deformation ε_{cs} for concrete of the compressive strength class B25 ... B65 and standard cone draft up to 7 cm is taken equal to (270 ... 400) · 10⁻⁵. The values of the coefficient φ_w , which takes into account the relative humidity of the outside air by the beginning of concrete drying, are determined in the same way as in the calculation of concrete creep deformations.

The values of concrete shrinkage deformations are calculated by the formula

$$\varepsilon_{cs} = 0.125 \cdot 10^{-6} \cdot w \cdot \sqrt{w} \quad (1.3)$$

Humidity deformation of concrete shrinkage in a cold, more humid season, taking into account the reversible moisture swelling deformation, if necessary, can be considered as the difference between concrete shrinkage deformation ε_{cs} determined by formula (1.3) and swelling deformations calculated by the formula:

$$\varepsilon_w = \alpha_w \cdot \Delta w \cdot \varphi \quad (1.4)$$

where α_w - seasonal moisture deformations of concrete swelling,

φ - coefficient, taking into account the scale factor, for seasonal moisture deformations of concrete swelling, is taken according to Table. 1.5 /2.3/.



Table 1.5

The values of the coefficient φ depending on the reduced element section height h_{red}						
3,5	5,0	10,0	20,0	30,0	40	50
1,1	1,0	0,9	0,75	0,55	0,40	0,35

The limiting values of deformations of moisture shrinkage of concrete can also be taken from Table. 1.6 depending on the relative humidity of the outside air and the reduced section height.

Table 1.6

Humidity of the hottest month %	Values of limiting shrinkage strains ε_{cs1} [$\cdot 10$] ⁽⁻⁶⁾ of heavy concrete (OK-1-2 cm) for a structure not protected from solar radiation during alternate heating and cooling at, cm						
	3,5	5	10	20	30	50	100
0	800	720	630	585	570	560	550
20	710	630	540	490	475	460	445
40	615	540	450	400	380	365	340
60	530	450	360	310	290	270	240
75	460	380	290	240	220	200	160
90	390	310	220	170	160	155	150

Note.1. h_{red} - the reduced height of the section of the element, which characterizes the massiveness of the structures and is equal to the sectional area divided by 1/2 of its diameter in contact with air.

2. Shrinkage deformations should be multiplied by: 0.85 - for structures made of concrete of a class below B 25.

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